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# Harmonics Reduction Techniques in Renewable Energy Interfacing Converters

Ali M. Eltamaly, Ph.D  
King Saud University  
Saudi Arabia

## 1. Introduction

In the recent years there has been growing interest in renewable energy generation along with growing demands for development of a suitable utility interface system. Low harmonics in the line currents of the converters used in the utility interface of the renewable energy system is the highest challenge. Controlled and uncontrolled converters are used widely in the utility interface of renewable energy systems to reduce cost, harmonic contents in line currents and to increase the reliability. These converters suffer from high level of Total Harmonic Distortion (THD) in the utility line currents which creates a lot of problems in the power system. A detailed third harmonic current injection technique has been introduced in details to reduce the harmonic contents in line currents of controlled and uncontrolled converters that used in renewable energy applications. The approach is based on circulating third harmonic current from DC link current to line currents of controlled and uncontrolled converters to reduce its THD. A new injected current shape is computed from analysis to achieve sinusoidal utility line currents. A controllable single switch boost converter connected in shunt is employed to circulate the new injected current shape. A method to implement the proposed approach under varying load condition is shown. Analysis, design, limitations, simulation and experimental result are presented.

In modern power electronics converters, three-phase controlled converter is commonly used especially as a rectifier or as an inverter in interfacing renewable energy systems with electric utility (Naik et al., 1995; Mohan, 1992, and Eltamaly, 2008). Three-phase controlled converter has simple construction and control, low cost, and low acoustic noise compared with other solutions like a full-bridge IGBT line side inverters or with Vienna rectifiers. Line current of controlled converter and its FFT components are shown in Fig. 1. It is clear from this waveform that this converter generates high harmonics in the line currents which distort the voltage at the point of common coupling in the power system. A lot of efforts have been performed to reduce harmonic contents in the utility line currents of controlled converter (Pacheco et al., 1994 – Arrillaga et al., 2006). Passive filters have been used in many researches with different configurations (Pacheco et al., 1994 and Bhattacharya et al., 1993), but this technique suffers from bulky, heavy filter elements and sometimes causes resonance problems. Active filters have been used in many researches and it sounds an

interesting option but this technique suffers from complexity and high cost (Ortega et al., 2005 and Lin & Ou, 2004). Hybrid solutions using active filters and passive filters in high power applications for improving passive filter performance (Bhattacharya et al., 1997). Increasing number of pulses (Lee et al., 1997 – Tinsley, 2003) reduces the harmonic contents in line current but this technique needs large in size, heavy in weight, high in cost, complex construction, and it will not be ready available from manufacturer (Lee, 1998). Early work in third harmonics injection techniques have been used in (Mohan, 1992 & Bhattacharya et al., 1993 and Arrillaga et al., 2006). Some other literatures use switches in the main pass of power flow which increase the switching losses and reduce the system reliability (Naik et al., 1995). Injection of third harmonic current to line currents can be achieved by using LC branches tuned around third harmonic frequency (Arrillaga et al., 2006). But, this scheme suffers from bulky construction, resonant problems, and the current in the injection branch is very sensitive to the deviation of L and C values. Most of three phase line current harmonics reduction techniques are summarized in (Mao et al., 19987 and Singh et al., 2004). Injection of third harmonic to line current using zigzag transformer has been shown in many researches and (Naik et al., 1995 and Pejovic, 2000). These researches and the ideas shown in this research show the superiority of this technique in reducing the harmonic contents of line currents and increasing the power factor of the controlled or uncontrolled converters.

## 2. Proposed Approach

Figure 2 shows the topology of the proposed approach to reduce harmonics generated by line commutated thyristor inverter used in interfacing renewable energy sources with electric utility. This approach contains a zigzag transformer that presents high impedance for fundamental frequency component and very low impedance for the injection current. A single-phase transformer is connected between the dc-link mid-point 'o' and the zigzag transformer neutral 'n'. The secondary of single-phase transformer is connected to a rectifier boost converter stage feeding the dc link. By operating single switch the injected current  $I_f$  can be regulated. The duty ratio of the boost converter is varying to control the injection current to be depending on the dc link voltage.

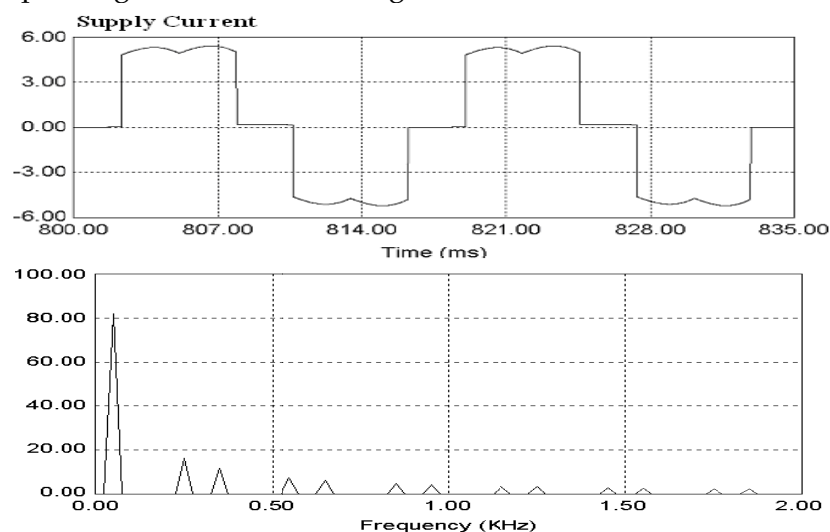


Fig. 1. Supply current and its FFT of controlled converter without harmonic reduction.

The optimal rms value and phase angle of injection current to get the minimum THD of supply current is the main issue in this chapter. Previous results say; the best rms value of 3rd harmonic current is equal to the average value of dc link current (Choi et al., 1996 and Lee, 1998). But it is not the only condition required, however, the angle of injection current plays a very important rule in the THD of the line current. So, it is important to determine the relation between the angle of injection current and the firing angle  $\alpha$ .

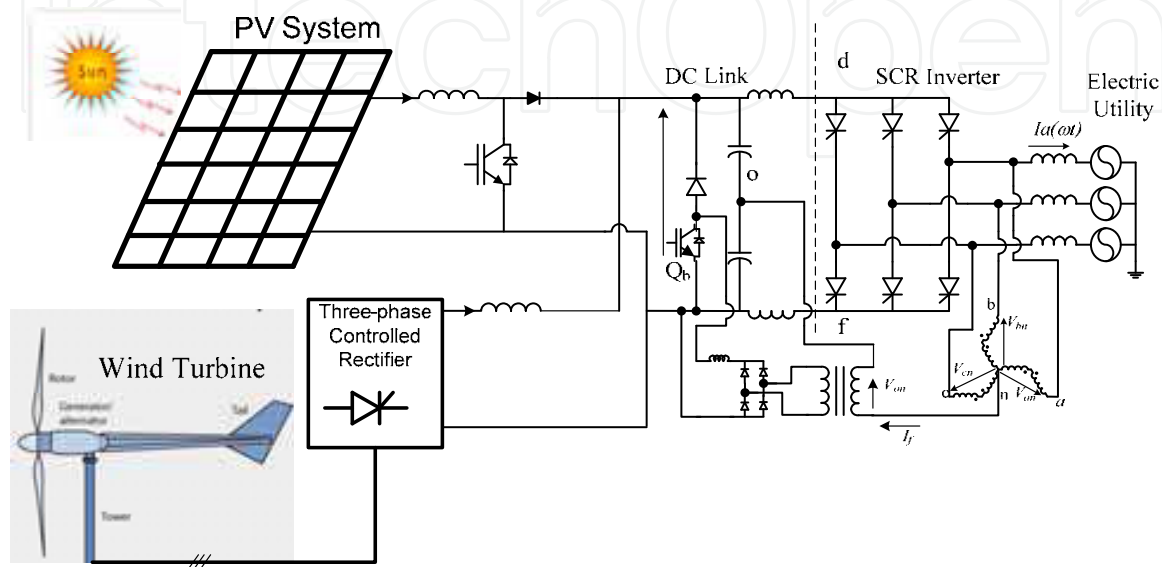


Fig. 2. The proposed approach

For firing angle  $\alpha = 20^\circ$  (as an example), Fig. 3 (a) shows the utility line current with respect to the voltage of phase 'a'. In Fig. 3 (b), the 3<sup>rd</sup> harmonic injection current with respect to phase 'a' voltage. It is clear from this waveform that the injection current leads the phase 'a' voltage by  $120^\circ$  which agree with the analysis and waveforms in the upcoming sections. In Fig. 3(c); the line current with using the 3<sup>rd</sup> harmonic current along with the phase voltage 'a'. This figure reveals that the angle between  $I_f$  and  $I_a$  must be  $180^\circ$  with respect to 3<sup>rd</sup> harmonic frequency. In Fig. 3(d) the voltage between point 'd' and 'n'  $V_{dn}$ , the voltage between point 'f' and 'n'  $V_{fn}$  and the voltage between 'o' and 'n'  $V_{on}$  along with phase 'a' voltage. The third harmonic components of the voltages  $V_{dn}$ ,  $V_{fn}$  and  $V_{on}$  have been used to inject third harmonic back to utility line current to reduce the harmonic contents in utility line currents. So a careful analysis for these voltages is required to get the optimum value of injection current and its angle. It is convenient to employ Fourier series in the analysis of the distorted waveforms. In general, a non-sinusoidal waveform  $f(\omega t)$  can be expressed as follows:

$$f(\omega t) = a_0 + \sum_{n=1}^{\infty} (a_n \cos(n\omega t) + b_n \sin(n\omega t))$$

where  $a_0$ ,  $a_n$ , and  $b_n$  are Fourier coefficients.

By applying Fourier equations to the waveforms of  $V_{dn}$  only to get the third harmonic component as following:

$$a_3 = \frac{3}{\pi} \int_{\frac{\pi}{6}+\alpha}^{\frac{5\pi}{6}+\alpha} V_m \sin \omega t * \cos 3\omega t \, d\omega t = \frac{3\sqrt{3} V_m}{8\pi} [2\sin(2\alpha) - \sin(4\alpha)] \quad (1)$$

$$b_3 = \frac{3}{\pi} \int_{\frac{\pi}{6}+\alpha}^{\frac{5\pi}{6}+\alpha} V_m \sin \omega t * \sin 3\omega t \, d\omega t = \frac{3\sqrt{3} V_m}{8\pi} [\cos(4\alpha) - 2\cos(2\alpha)] \quad (2)$$

From (1) and (2),  $V_{dn3}$  and its angle can be obtained as in (3) and (4).

$$V_{dn3} = \frac{1}{\sqrt{2}} * \sqrt{a_3^2 + b_3^2} = \frac{3V_{LL}}{8\pi} \sqrt{1 + 8\sin^2 \alpha} \quad (3)$$

where:  $V_m$  is the peak value of phase voltage,

$V_{LL}$  is the rms value of line to line supply voltage, and,

$V_{dn3}$  is the rms value of 3<sup>rd</sup> harmonic of the voltage between points  $d$  and  $n$ .

And angle of  $V_{dn3}$  is

$$\tan^{-1} \left( \frac{a_3}{b_3} \right) = \tan^{-1} \left( \frac{2\sin(2\alpha) - \sin(4\alpha)}{\cos(4\alpha) - 2\cos(2\alpha)} \right) \quad (4)$$

In the same way  $V_{fn3}$  can be obtained as following:

$$a_3 = \frac{3}{\pi} \int_{\frac{7\pi}{6}+\alpha}^{\frac{11\pi}{6}+\alpha} V_m \sin \omega t * \cos 3\omega t \, d\omega t = \frac{3\sqrt{3} V_m}{8\pi} [2\sin(2\alpha) - \sin(4\alpha)] \quad (5)$$

$$b_3 = \frac{3}{\pi} \int_{\frac{7\pi}{6}+\alpha}^{\frac{11\pi}{6}+\alpha} V_m \sin \omega t * \sin 3\omega t \, d\omega t = \frac{3\sqrt{3} V_m}{8\pi} [\cos(4\alpha) - 2\cos(2\alpha)] \quad (6)$$

From (5) and (6),  $V_{fn3}$  and its angle as in (7) and (8).

$$V_{fn3} = \frac{1}{\sqrt{2}} * \sqrt{a_3^2 + b_3^2} = \frac{3V_{LL}}{8\pi} \sqrt{1 + 8\sin^2 \alpha} \quad (7)$$

$V_{fn3}$  is the rms value of 3<sup>rd</sup> harmonic of the voltage between points  $f$  and  $n$ .

And angle of  $V_{fn3}$  is;

$$\tan^{-1} \left( \frac{a_3}{b_3} \right) = \tan^{-1} \left( \frac{2\sin(2\alpha) - \sin(4\alpha)}{\cos(4\alpha) - 2\cos(2\alpha)} \right) \quad (8)$$

$$V_{on3} = \frac{V_{dn3} + V_{fn3}}{2} \quad (9)$$

Then;

$$V_{on3} = \frac{3V_{LL}}{8\pi} \sqrt{1 + 8\sin^2 \alpha} \quad (10)$$

And angle of  $V_{on3}$ , is

$$\theta = \tan^{-1} \left( \frac{a_3}{b_3} \right) = \tan^{-1} \left( \frac{2\sin(2\alpha) - \sin(4\alpha)}{\cos(4\alpha) - 2\cos(2\alpha)} \right) \quad (11)$$

The 3<sup>rd</sup> harmonic injection current is;

$$I_f \angle \varphi = \frac{V_{on3} \angle \theta}{Z \angle \psi} = \frac{V_{on3}}{Z} \angle (\theta - \psi) \quad (12)$$

where,  $V_{on3}$  is the rms value of 3<sup>rd</sup> harmonic of the voltage between points  $o$  and  $n$ , and,  $\theta$  is the angle of  $V_{on3}$ , and,  $\psi$  is the angle between  $V_{on3}$  and  $I_f$  (the impedance angle of injection current path).

As shown in Fig. 3, the voltage  $V_a$  is taken as a reference, so the phase angle of fundamental and 3<sup>rd</sup> harmonic components of phase  $a$  current are  $-\alpha$  and  $-3\alpha$  respectively. As explained in (Eltamaly, 2003) and it is clear from Fig. 3, the optimum phase difference between phase  $a$  current and injection current is  $180^\circ$ . Then the difference between the angle of  $I_f$  (which is  $\phi$ ) and the angle of fundamental current which is  $(-\alpha$  and  $-3\alpha$  for fundamental and third harmonic frequencies respectively) is  $180^\circ$  as described in (13).

$$(\varphi_{opt}) - (-3\alpha) = 180 \quad (13)$$

So the optimum angle of the injection current,  $\phi_{opt}$  can be obtained from the following equation;

$$(\varphi_{opt}) = 180 - 3\alpha \quad (14)$$

Also, the optimum angle of the impedance of injection current path,  $\psi_{opt}$  can be obtained from the following equation;

$$\psi_{opt} = \theta + 3\alpha - 180 \quad (15)$$

From (14) and (15) the phase difference between each vectors for various firing angles;  $\alpha = 20^\circ$  and  $40^\circ$  (as an example for rectifier mode) and  $\alpha = 130^\circ$  and  $150^\circ$  (as an example for inverter mode) is shown in Fig. 4 (a) and (b) respectively. From (10) the relation between  $V_{on3}/V_{LL}$  and the firing angle  $\alpha$  is shown in Fig. 5. In the same way; from (14) and (15) the variation of injection current optimum angle, the angle of  $V_{on3}$ ,  $\theta$  and the angle between  $I_f$  and  $V_{on3}$  (angle of impedance angle of injection path) along with the firing angle  $\alpha$  is shown in Fig. 5.



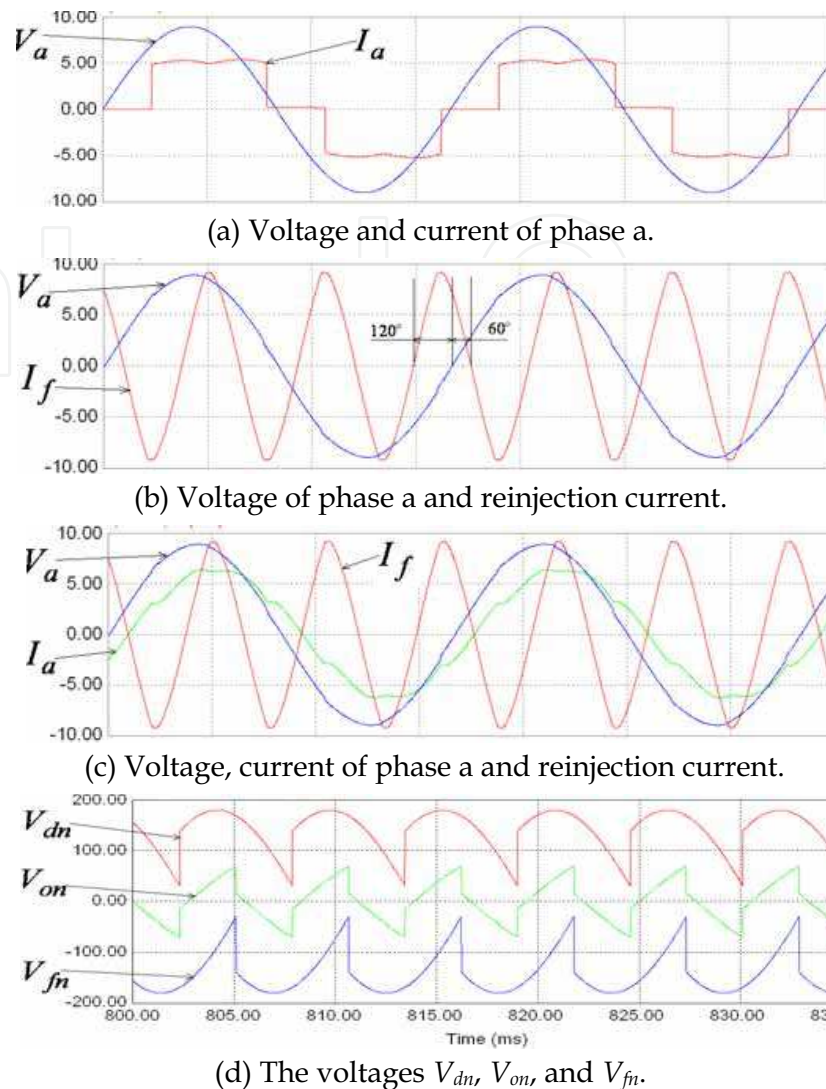


Fig. 3. Various voltages and currents of the proposed approach at  $\alpha=20^\circ$ .

### 3. Design Example

Experimental and simulation verification for this technique has been carried out. The prototype model is used in simulation and in the experiment. DC link is connected to three-phase controlled converter and electrical utility as shown in Fig. 2. For the controlled rectifier, the values of  $V_{on3}$  varies between  $V_{on3}(\alpha=0)=0.1194\text{pu}$  to  $V_{on3}(\alpha=90^\circ)=0.358\text{pu}$ . At full load the dc current  $I_o=0.6224\text{ pu}$ . The base voltage and current are 220V and 3.3A, respectively.

The simulation results in the next section reveals that the minimum THD occurs almost at  $I_f/I_o=1.15$ , so at full load;  $I_f=0.716\text{pu}$ . The rated third harmonic current passing through zigzag transformer is  $I_f/3=0.239\text{pu}$ . The value of  $I_f$  is controlled depending on the value of dc link current for minimum THD. The third harmonic injection current can be controlled by controlling the duty ratio of the boost converter. Current sensor is used to measure the

actual dc link current and the 3<sup>rd</sup> harmonic injection current. The error signal between these two currents is used to control the duty ratio of the boost converter. 10 kHz switching frequency of the boost converter is used in simulation and in the practical prototype. The schematic of the controlled circuit of the boost converter is shown in Fig. 6.

### Design of Single-Phase Transformer

The rated primary voltage of single phase transformer in 3<sup>rd</sup> harmonic injection pass is  $V_{on3}(\alpha = 90) = 0.358 \text{ pu}$ . Also the rated primary current of this transformer is  $I_f = 0.716 \text{ pu}$ . So, the rated kVA of this transformer is  $0.716 * 0.358 = 0.256 \text{ pu}$ .

The turns ratio of step up single-phase must handle the minimum value as well as the maximum value of  $V_{on3}$ . The minimum value of  $V_{on3}$  is at  $\alpha = 0$  which is  $V_{on3}(\alpha = 0) = 0.1194 \text{ pu}$ . Then, the corresponding value of  $V'_{on3}$  is:

$$V'_{on3}(\alpha = 0) = 0.1194 / n \text{ pu} \quad (16)$$

The output dc voltage of single-phase diode rectifier,  $V_{bi}$  is:

$$V_{bi} = 2 * \sqrt{2} * V'_{on} / \pi \quad (17)$$

The minimum value of  $V_{on3}$  is corresponding on the maximum value of the duty ratio of boost converter. Assume the maximum allowable value of the duty ratio is 0.8. Then the output voltage of the boost converter,  $V_{bo}$  is:

$$V_{bo} = V_{bi} / (1 - D) \quad (18)$$

Substitute the value of  $V_{bi}$  from (17) into (18) and  $D=0.8$ , the following equation can be obtained:

$$V_{bo}(D = 0.8) = (2 * \sqrt{2} * V'_{on} / \pi) / (1 - 0.8) = (10 * \sqrt{2} * V'_{on}) / \pi \quad (19)$$

The output voltage from the boost converter must equal the dc link voltage. The dc link voltage is kept constant at 1.15 pu by controlling the firing angle of the controlled converter and the modulation index of PWM inverter. So, by equating (19) with 2.2pu, the following equation can be obtained:

$$10 * \sqrt{2} * V'_{on3} / \pi = 2.2 \text{ pu},$$

Then;

$$V'_{on3}(\alpha = 0) = 2.2 * \pi / (10\sqrt{2}) \text{ pu} \quad (20)$$

By equating the values of  $V'_{on3}$  in (14) and (18), the following equation can be obtained:

$$0.1194 / n = 2.2 * \pi / (10\sqrt{2})$$

Then the turns ratio of the single-phase transformer is:

$$n = 10\sqrt{2} * 0.1194 / (2.2 * \pi) = 0.24 \quad (21)$$



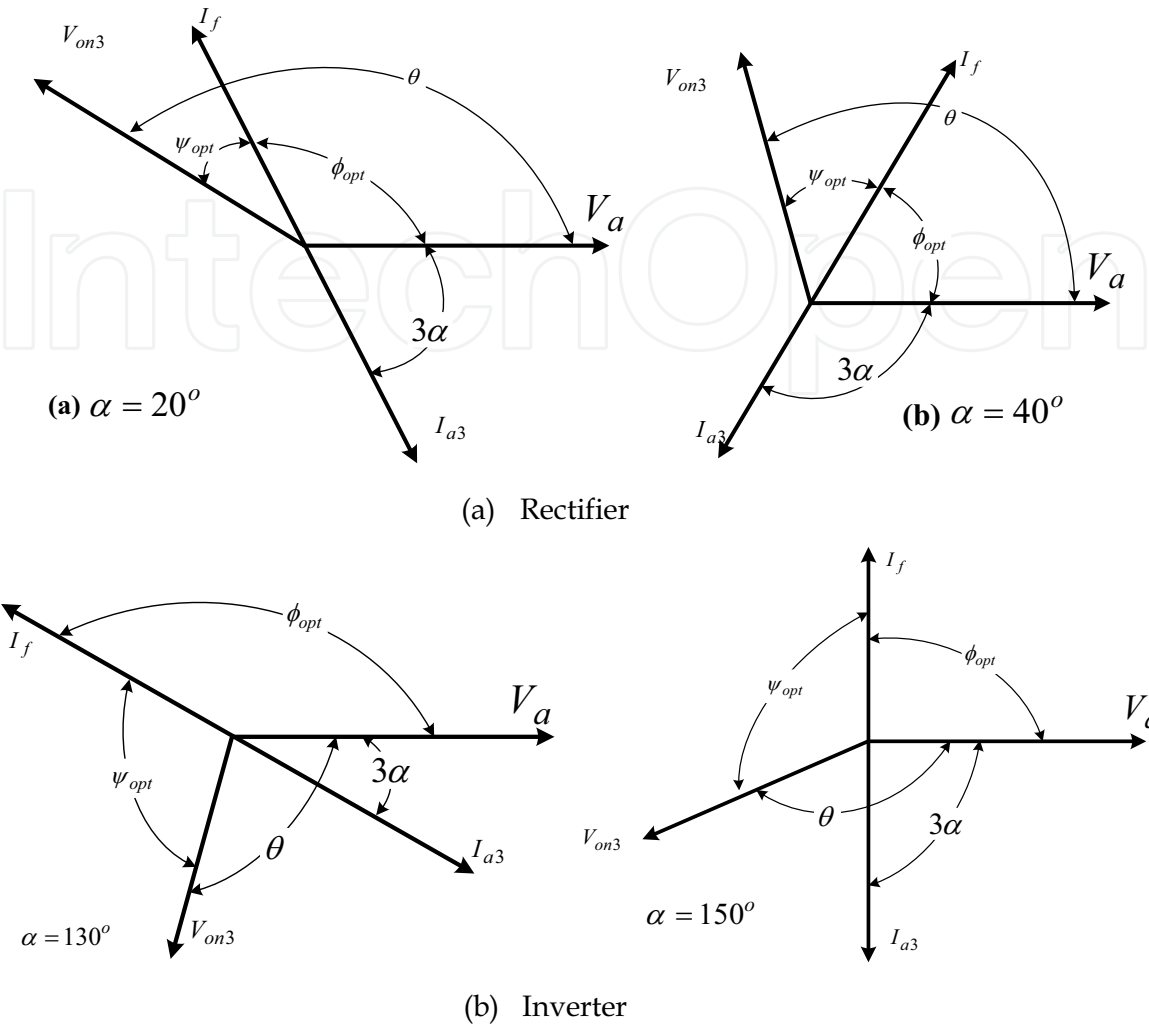


Fig. 4. Phase difference between each component in a rectifier and inverter

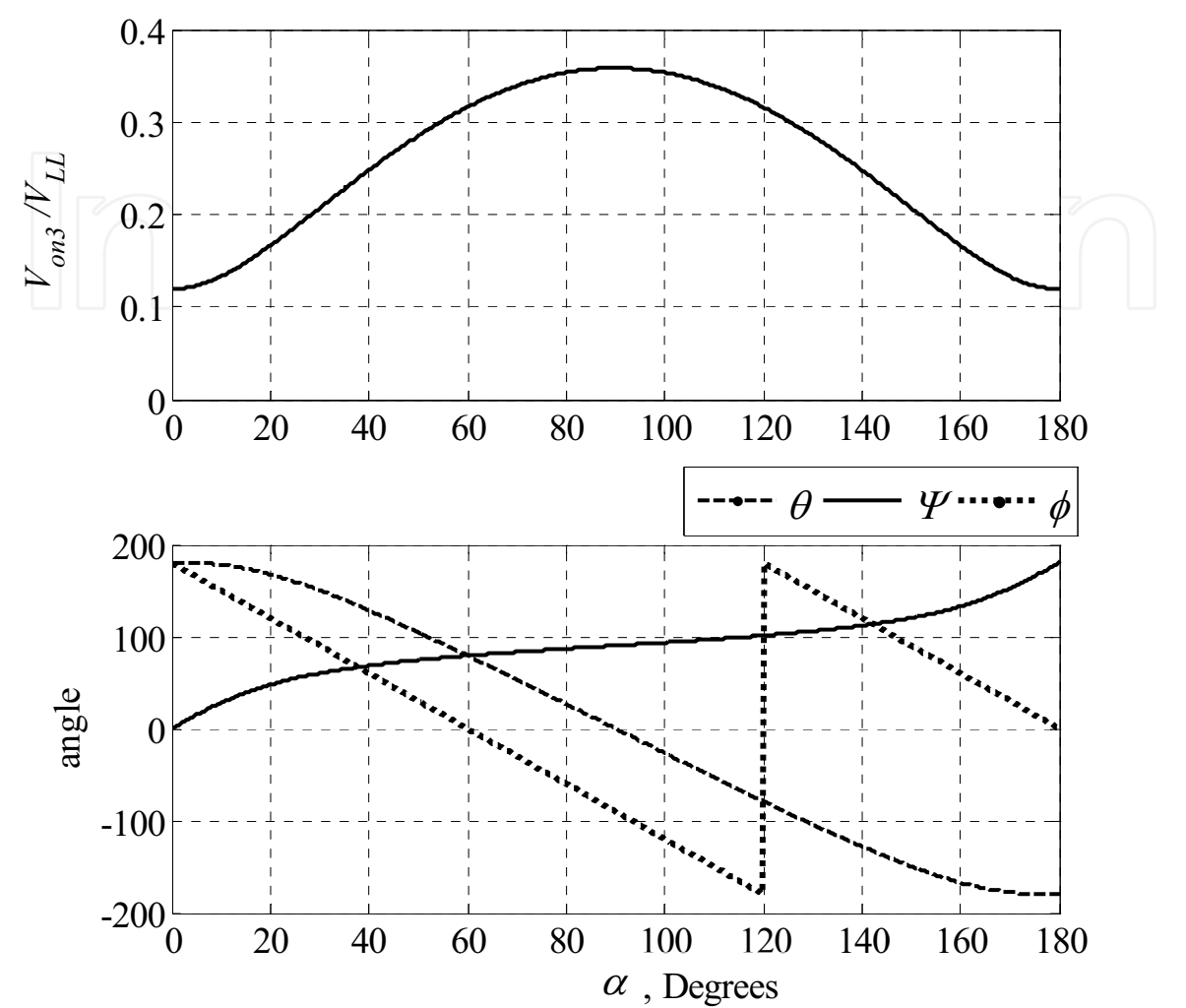


Fig. 5. The variation of  $V_{on3}$ ,  $\theta$ ,  $\phi_{opt}$ ,  $\psi_{opt}$  along with  $\alpha$ .

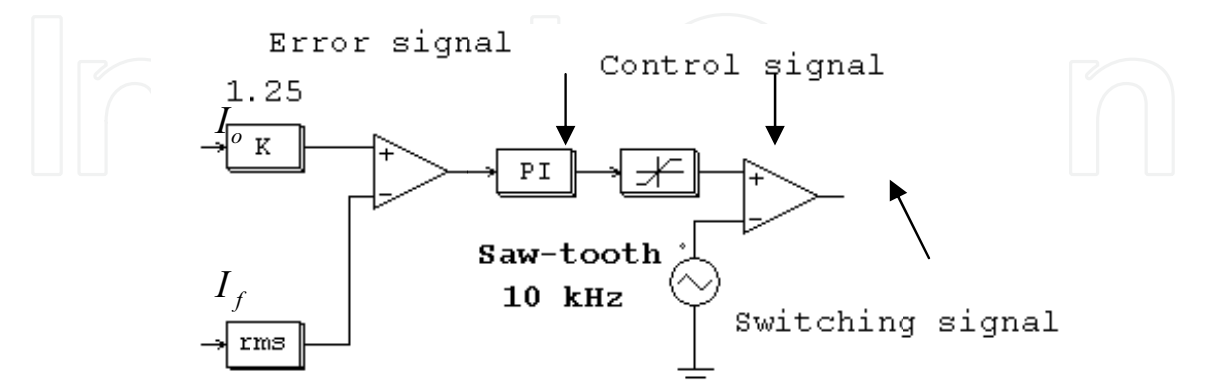


Fig. 6. The schematic of the control circuit of the boost converter.

#### 4. Simulation and Experimental Results

The simulation of the proposed technique has been performed by using PSIM computer program (PSIM6.1). Same values of the components used in simulation program have been used in the experimental prototype to compare these results.

Fig. 7 shows the relation between THD and the value of  $I_f/I_o$  for different values of firing angle,  $\alpha$ . This figure reveals that the optimal value of  $I_f/I_o$  is about 1.15 for the best THD. Also, This figure shows the importance of 3<sup>rd</sup> harmonic injection technique especially for high value of firing angle,  $\alpha$ .

Fig. 8 shows the relation between THD and the angle of  $I_f$  with respect to  $V_{on}$ ,  $\psi$  at  $I_f/I_o=1.15$  for different values of firing angle,  $\alpha$ . It is clear that the best THD occurs around  $\psi_{opt}$  which obtained from (13). The value of  $\psi_{opt}$  increase with increasing the firing angle  $\alpha$ .

The simulation and experimental waveforms are shown for  $\alpha=20^\circ$  and  $40^\circ$  as an examples.

##### 4.1 Simulation and experimental results at $\alpha=20^\circ$

Figure 9 shows the waveforms of voltage  $V_{df}$  and  $V_{ab}$ . Fig. 10 shows the supply current waveform and its FFT components with respect to phase  $a$  voltage without injection of 3<sup>rd</sup> harmonic current. It is clear from this figure that the supply current has very high THD mostly of 5<sup>th</sup> and 7<sup>th</sup> harmonics. Fig. 11 shows the voltage of  $V_{dn}$ , and  $V_{fn}$ . It is shown in the top of the experimental result waveform that the frequency of this voltage is  $180^\circ$  which is the 3<sup>rd</sup> harmonic voltage and the value of rms voltage is 39.9 that can be obtained from (10) at  $\alpha=20^\circ$ . Figure 12 shows the supply current waveform and its FFT components with respect to phase  $a$  voltage with optimum amplitude and angle of 3<sup>rd</sup> harmonic current injection. It is clear from this figure that the supply current becomes very near to sine-wave with 5% THD.

Figure 13 shows supply current waveform  $I_a$  and optimum value and angle of injection 3<sup>rd</sup> harmonic current with respect to phase  $a$  voltage. It is clear from these waveforms that the value of the angle between  $I_f$  and  $V_a$  is about  $120^\circ$  and the angle between  $I_a$  and  $I_f$  is  $180^\circ$  which agree with the vector diagram shown in Fig. 4 (a).

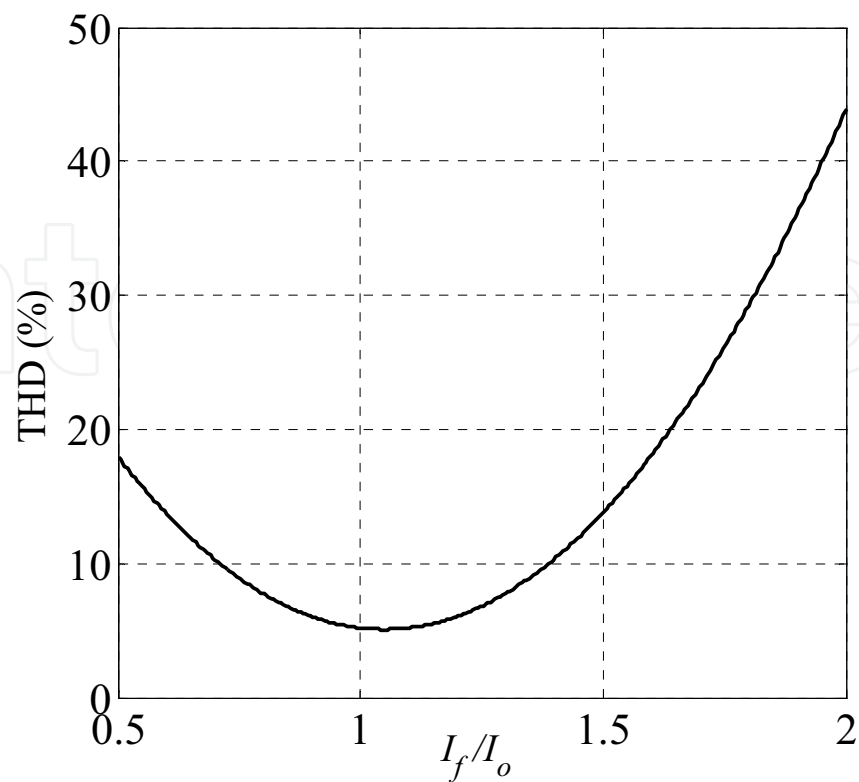


Fig. 7. The relation between THD and the value of  $I_f/I_o$ .

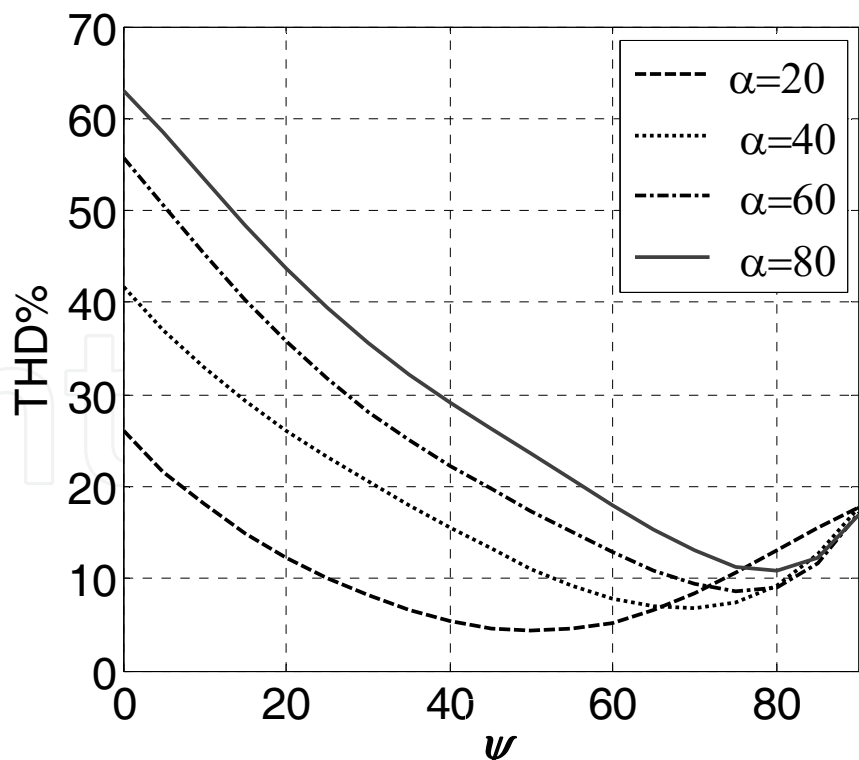


Fig. 8. The relation between THD and the angle of  $I_f$  with respect to  $V_{on}$  at  $I_f/I_o=1.15$  for different values of firing angle,  $\alpha$ .

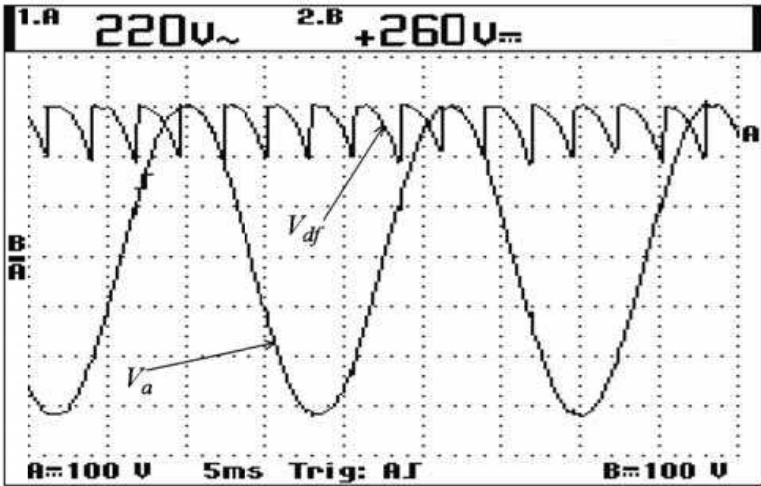


Fig. 9. The waveforms of voltage  $V_{df}$  and  $V_{ab}$ .

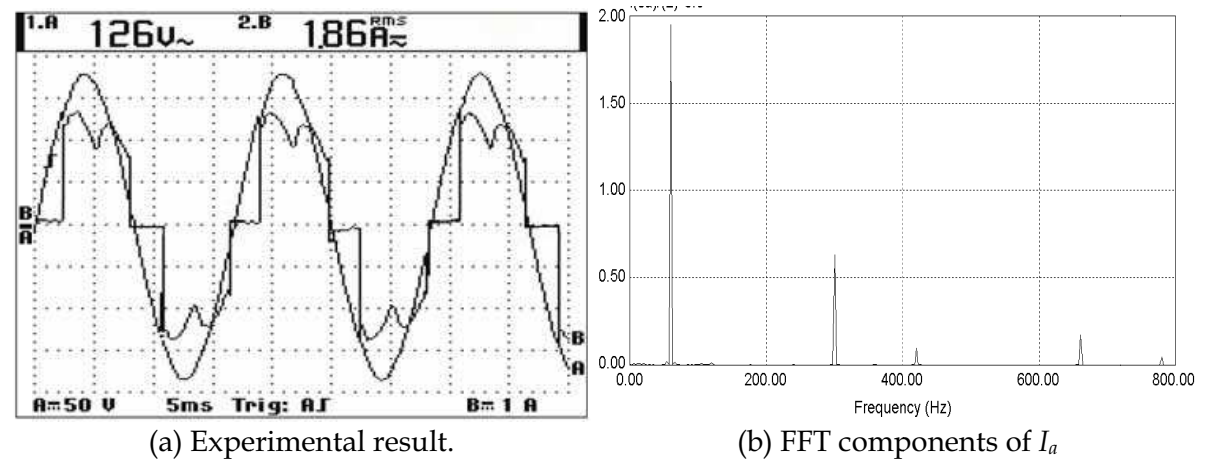


Fig. 10. The supply current waveform and its FFT components with respect to phase  $a$  voltage without injection of 3<sup>rd</sup> harmonic current.

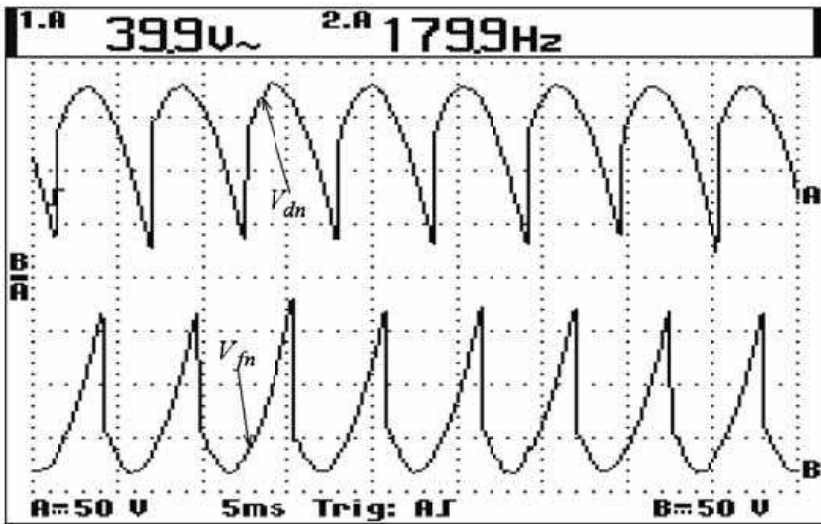
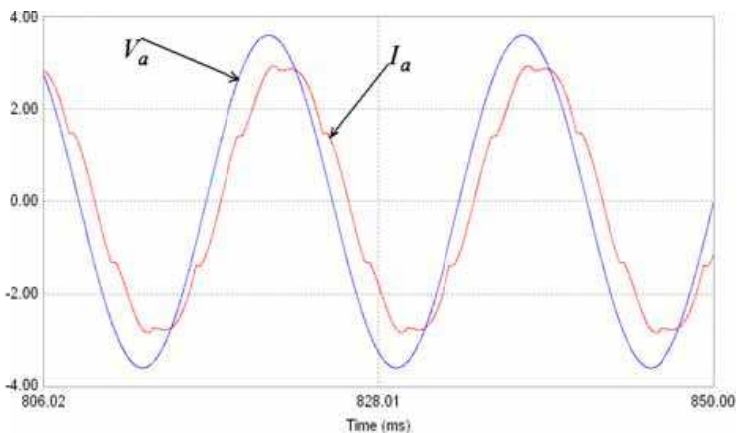
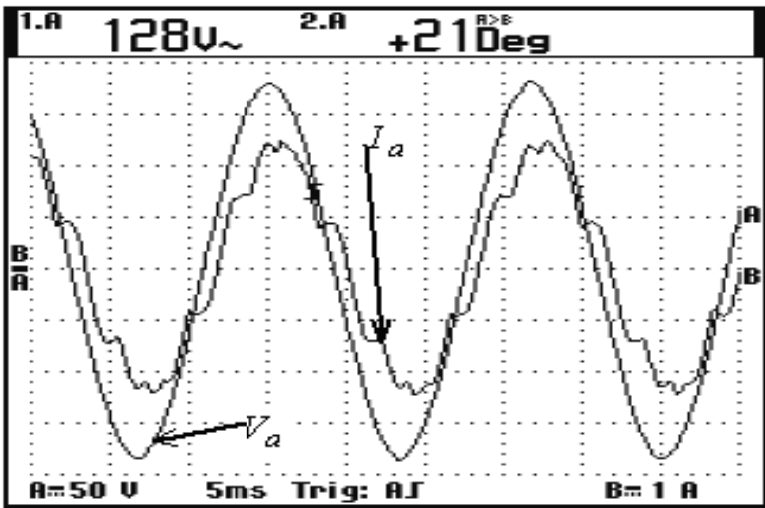


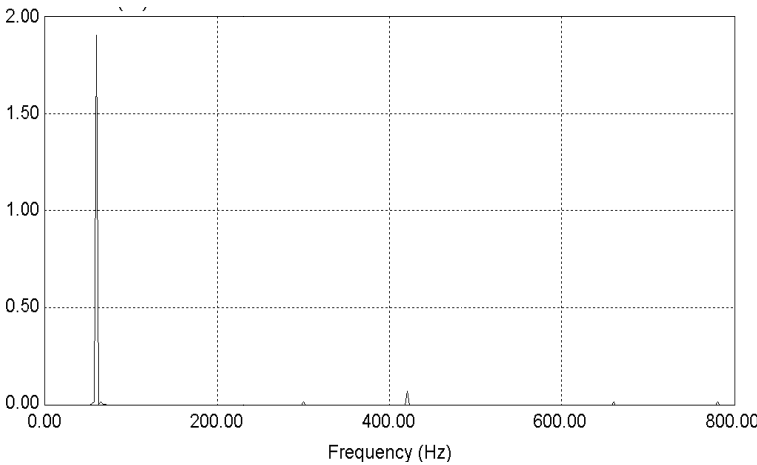
Fig. 11. The voltage of  $V_{dn}$ , and  $V_{fn}$



(a) Simulation result.



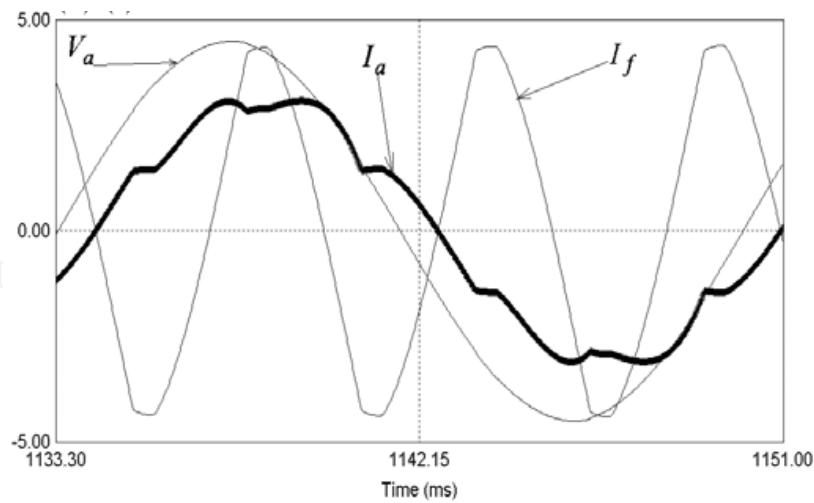
(b) Experimental result.



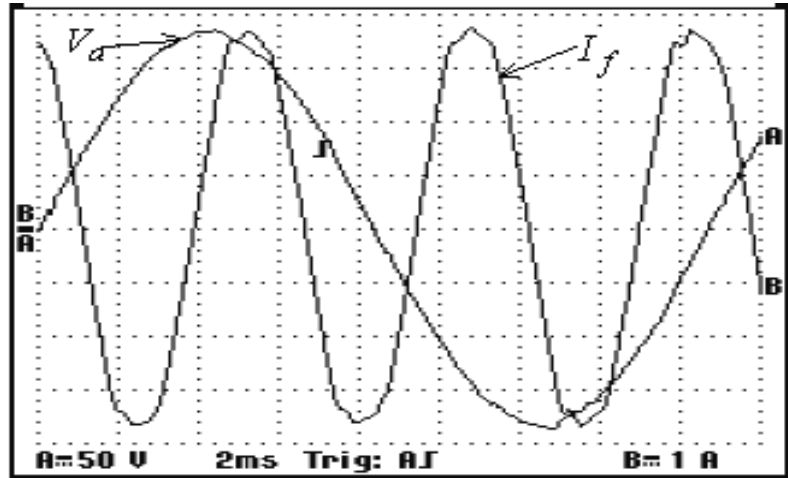
(c) FFT components of  $I_a$ .

Fig. 12. The supply current waveform and its FFT components with respect to phase  $a$  voltage at optimum 3<sup>rd</sup> harmonic current injection.

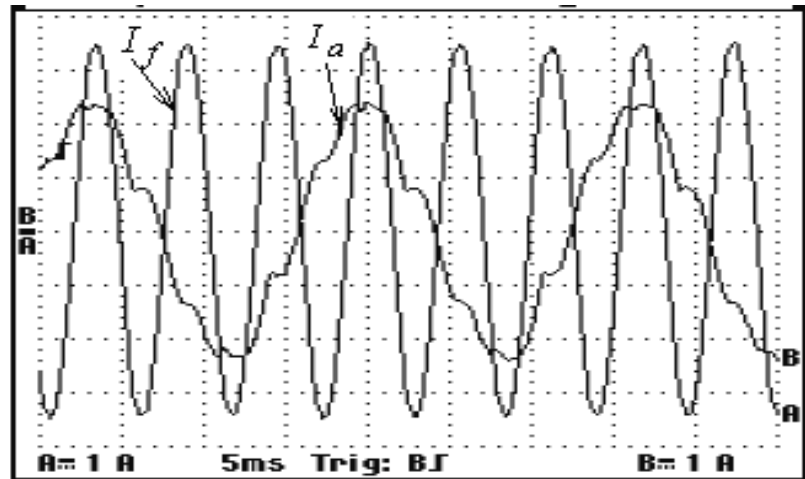




(a) Simulation result for  $V_a$  and  $I_f$ .



(b) Experimental result for  $V_a$  and  $I_f$ .



(c) Experimental result for  $I_a$  and  $I_f$ .

Fig. 13. The supply current waveform  $I_a$  and optimum value and angle of injection 3<sup>rd</sup> harmonic current with respect to phase  $a$  voltage.

#### 4.2 Simulation and experimental results at $\alpha=40^\circ$

Figure 14 shows the waveforms of voltage  $V_{df}$  and  $V_{ab}$ . Fig. 15 shows the supply current waveform and its FFT components along with phase  $a$  voltage without injection of 3<sup>rd</sup> harmonic current. It is clear from this figure that the supply current has very high THD mostly of 5<sup>th</sup> and 7<sup>th</sup> harmonics. It is clear that this THD is high than the one of  $\alpha=40^\circ$ .

Figure 16 shows the voltage of  $V_{dnr}$  and  $V_{fn}$  and their FFT components with respect to phase  $a$  voltage. It is clear from this figure that these voltages have triplex harmonics and the 3<sup>rd</sup> harmonic is the most dominant harmonic. It is also clear that both voltages  $V_{dnr}$  and  $V_{fn}$  have the same harmonics.

Figure 17 shows supply current waveform and its FFT components with optimum value and angle of injection 3<sup>rd</sup> harmonic current. It is clear from this figure that the supply current becomes very near to sine-wave with 6% THD.

Figure 18 shows the supply current waveform  $I_a$  and optimum value and angle of 3<sup>rd</sup> harmonic injection current with respect to phase  $a$  voltage. It is clear from these waveforms that the angle between  $I_f$  and  $V_a$  is about  $60^\circ$  which agree with the vector diagram in Fig. 4 (b).

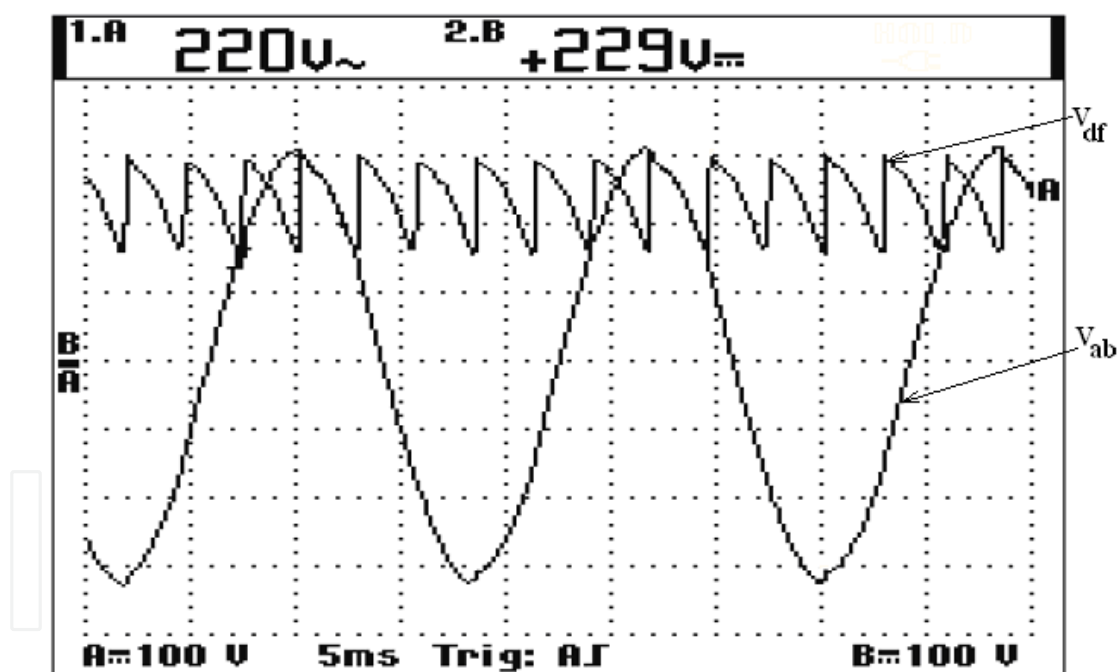


Fig. 14. The waveforms of voltage  $V_{df}$  and  $V_{ab}$ .

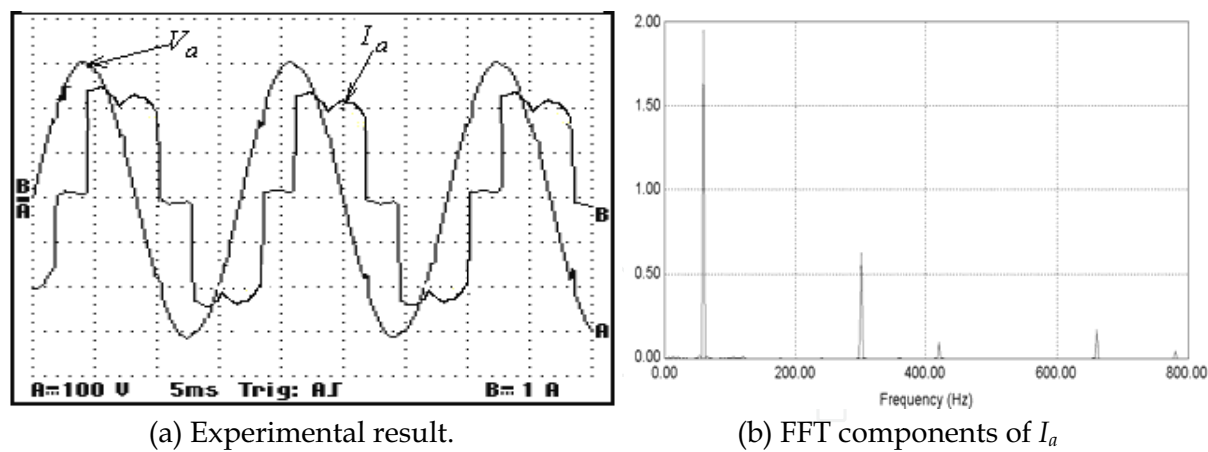


Fig. 15. The supply current waveform and its FFT components along with phase a voltage without injection of 3<sup>rd</sup> harmonic current.

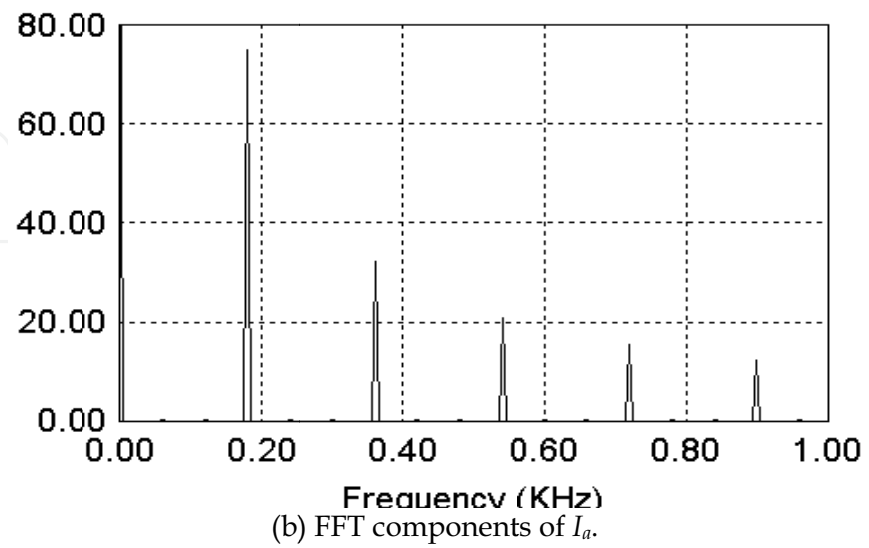
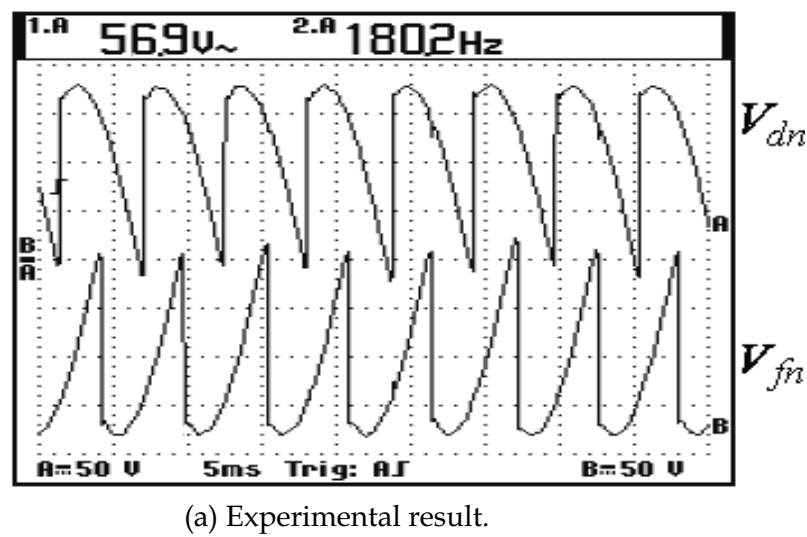


Fig. 16. The voltage of  $V_{dn}$  and  $V_{fn}$  and their FFT components with respect to phase  $a$  voltage.

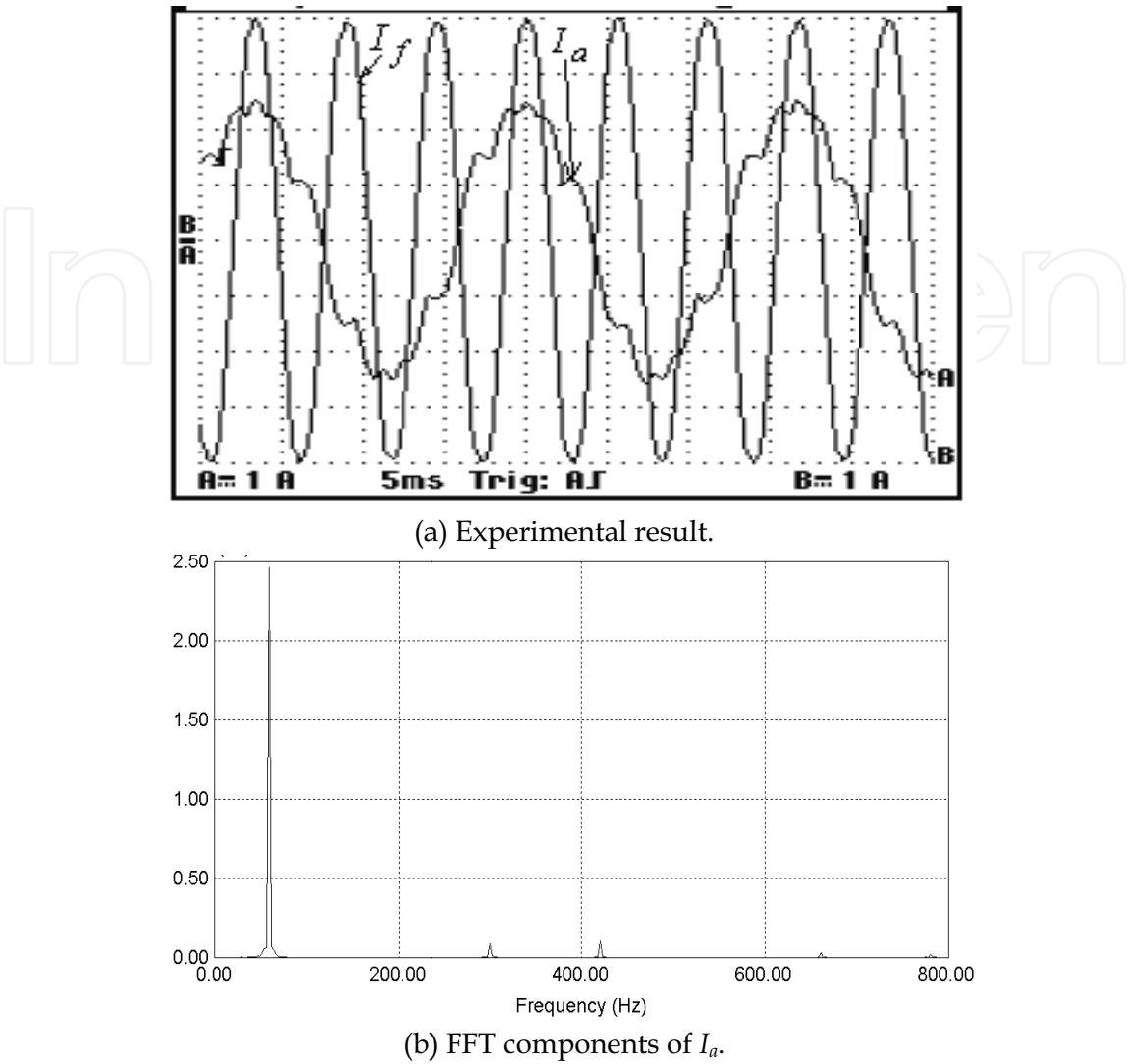


Fig. 17. The supply current waveform and its FFT components with optimum value and angle of injection 3<sup>rd</sup> harmonic current.

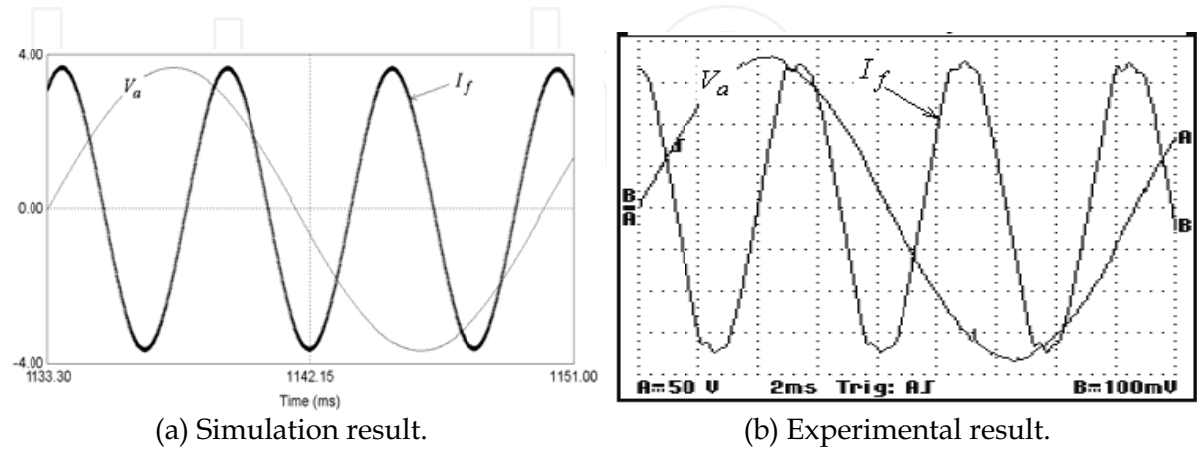


Fig. 18. The supply current waveform  $I_a$  and optimum value and angle of injection 3<sup>rd</sup> harmonic current with respect to phase  $a$  voltage.

#### 4. Conclusions

Third harmonics injection technique plays a significant rule in reducing of the THD of the utility line current of three-phase controlled converters. The optimal amplitude and phase angle of injection current slightly changes with the firing angle. In this research, a detailed analysis for determining the relation between the optimal amplitude and phase angle of injection current along with the firing angle has been carried out. The THD of line current is highly affected by the amplitude of 3<sup>rd</sup> harmonic injection current as well as its phase angle with supply voltage. The optimum amplitude and angle of 3<sup>rd</sup> harmonic current have been determined by a detailed mathematical analysis of the system. The THD of the utility line current from simulation and the experimental results proves the mathematical results for this technique. The THD of the utility line current with optimal harmonic injection current is lower than limits of harmonics standards.

#### 5. References

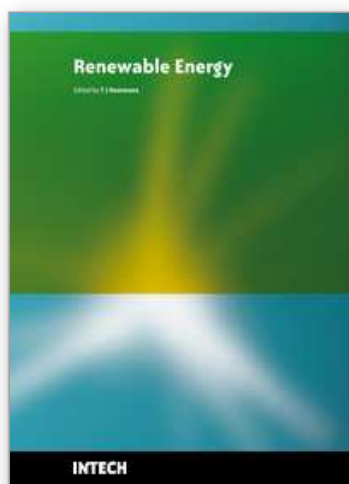
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51000 Rijeka, Croatia  
Phone: +385 (51) 770 447  
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Phone: +86-21-62489820  
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